

		Calculation Sheet				Job No.		Sheet No.		Rev.					
		-SEDIMENT TRAP -Catchment 20 ha				SB1									
						Member/Location :									
						Drg. Ref. :									
Job Title :		SEDIMENT TRAP				Made by		NAS		Date		13.11.2018		Remark	
		<b><u>SEDIMENT TRAP DESIGN</u></b>													
		<b>1 <u>Sizing a Wet Sediment Trap</u></b>													
		<b>Limitation in design</b>													
Table 12.15		Rain Fall				=		50.00		mm					
		<b><u>STAGE 1 - Completing Earthworks</u></b>													
		<b><u>Catchment Area</u></b>													
		Total Catchment Area				=		20		ha		Soil type :			
						=		200000		m2		Clay/Loam			
		Therefore design wet sediment basin. To provide wet sediment basin with earth embankment and emergency spillway.													
		<b><u>Assumptions</u></b>													
Table 12.16		<b>1</b> Most of the surface soil type is clay/Loam.													
Table 12.19		<b>2</b> Site runoff potential as : Moderate to high runoff for settling zone volume. Moderate to high runoff for total volume.													
Table 12.17		<b>3</b> Design Criteria of Sediment Basin for Sediment Control as per Table 12.17													
		<b>4</b> The temporary basin design life is 12 to 18 months.													

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Table 12.16	1 Sizing of sediment trap.																							
	The predominant soil type is categorised as HSG Type		C																					
	Rainfall		= 50.00 mm																					
Table 12.19	Settling zone volume		= 290 m <sup>3</sup> /ha																					
	Total volume		= 435 m <sup>3</sup> /ha																					
Table 12.17	(a) <u>Settling Zone Volume &amp; Total Volume</u>																							
	Wet Sediment Basin Sizing Guidelines,																							
	the nearest magnitud of design storm event in mm =		50.00 mm																					
	Therefore :																							
	Ave. Basin Surface area		=		290		m <sup>3</sup> /ha		x		20.0		ha		=		5800		m <sup>2</sup>		Req. Surface			
	Total Basin volume		=		435		m <sup>3</sup> /ha		x		20.0		ha		=		8700		m <sup>3</sup>		Req. Volume			
	(a) <u>Settling Zone</u>																							
	The Required settling zone, V <sub>1</sub>		=		4350.0		m <sup>3</sup>		(Half the Total Volume)															
	Minimum settling zone depth, y <sub>1</sub>		=		1.00		m												Note: min 0.6m					
	Try settling zone average width, W <sub>1</sub>		=		40.0		m																	
	The settling zone average length, L <sub>1</sub>		=		V <sub>1</sub>		=		4350.0		=		108.8		m		, say		180		m			
					W <sub>1</sub> x y <sub>1</sub>				40.0 x		1.00													
	Average Surface Area Provided		=		W <sub>1</sub> x L <sub>1</sub>		=		7200		m <sup>2</sup>		>		5800		→		OK!					
	Check settling zone dimensions,																							
	L <sub>1</sub> ratio		=		180		=		180		<		200		→		OK!							
	y <sub>1</sub>				1.00																			
	L <sub>1</sub> ratio		=		180		=		4.5		>		2.0		→		OK!							
	W <sub>1</sub>				40																			
	(b) <u>Sediment Storage Zone</u>																							
	The required sediment storage zone volume is Half the total volume, V <sub>2</sub>																							
V <sub>2</sub> = 1/2 x Total Volume																		= 4350		m <sup>3</sup>				
For a side slope z = 2 (H) : 1 (V), the dimensions at the top of the sediment storage zone are :																								
W <sub>2</sub> = W <sub>1</sub> - 2 (d <sub>1</sub> /2)(z)																		= 60.0		m				
L <sub>2</sub> = L <sub>1</sub> - 2 (d <sub>1</sub> /2)(z)																		= 120.0		m				

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Table 12.17		The required depth for the sediment storage zone, which must be at least 0.3m, can be calculated from the following relationship :															
		$V_2 = Z^2 Y_2^3 - Z Y_2^2 (W_2 + L_2) + Y_2 (W_2 L_2)$															
		which gives,															
		$4350 = (2)^2 Y_2^3 - (2) Y_2^2 (180.0) + Y_2 (7200.0)$															
		$= 4 Y_2^3 - (360.0) Y_2^2 + Y_2 (7200.0)$															
		use trial and error method to find $Y_2$ ,															
		For $Y_2 = 0.7$ m, $V_2 = 4865.0$ m <sup>3</sup>															
		For $Y_2 = 0.64$ m, $V_2 = 4461.6$ m <sup>3</sup>															
		For $Y_2 = 0.8$ m, $V_2 = 5531.6$ m <sup>3</sup>															
		$Y_2 = 0.640 > 0.300$ m minimum storage zone depth requirement															
		$V_2 = 4461.6 > 4350$ m <sup>3</sup> of sediment storage volume → OK!															
		( c ) Overall Basin Dimension															
		Base : $W_B = W_1 - 2 \times Z \times [y_1/2 + y_2]$ = 35.44 m say 35 m $L_B = L_1 - 2 \times Z \times [y_1/2 + y_2]$ = 175.4 m say 175 m															
		Depth : Settling zone $y_1 = 1.00$ m Sediment Storage Zone $y_2 = 0.64$ m															
		Side slope, Z = 2.0 (H): 1.0 (V)															

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<b>2 SIZING OF BASIN OUTLET</b>																							
The emergency spill way must be designed for a 10-yr ARI The Sill level must be set at minimum 300 mm above the basin top water level. Assumption :- i) Assume riser pipe flow is orifice flow through the top of the pipe only ii) Riser pipe head is 300mm, i.e the height between the top of the pipe and spillway crest level																							
$Q_{\text{Spillway}} = Q_{10} - Q_{\text{Riser}}$																							
<b>A) Determine of <math>Q_{10}</math></b>																							
Eqn. 2.2 $i = \frac{\lambda T^k}{(d+e)^n}$																							
where; i = the ave. rainfall (mm/hr) for selected ARI(T) and storm duration T = ave. recurrence interval, ARI (years) d = storm duration (hrs) ; $0.20 \leq d \leq 72$ λ, k, e and η = fitting constants dependent on the raingauge location																							
<table border="1"> <thead> <tr> <th rowspan="2">Location &amp; Station ID</th> <th rowspan="2">ARI, T (years)</th> <th rowspan="2">Storm Duration , d</th> <th colspan="4">Derived Parameters</th> </tr> <tr> <th>λ</th> <th>k</th> <th>e</th> <th>η</th> </tr> </thead> <tbody> <tr> <td>JPS Kemaman Jambatan</td> <td>10</td> <td>15</td> <td>75.8258</td> <td>0.2385</td> <td>0.3811</td> <td>0.7303</td> </tr> </tbody> </table>						Location & Station ID	ARI, T (years)	Storm Duration , d	Derived Parameters				λ	k	e	η	JPS Kemaman Jambatan	10	15	75.8258	0.2385	0.3811	0.7303
Location & Station ID	ARI, T (years)	Storm Duration , d	Derived Parameters																				
			λ	k	e	η																	
JPS Kemaman Jambatan	10	15	75.8258	0.2385	0.3811	0.7303																	
As Such;																							
$i = \frac{75.8258 \times 10^{0.2385}}{\left( \left( \frac{15}{60} \right) + 0.3811 \right)^{0.7303}} = 131.32 = 184 \text{ mm/hr}$																							
Section 2.3.1 Table 2.5 <b>Rational Method</b>																							
Coefficient of Runoff, C = 0.5 (Bare Soil)																							
Catchment Area, A = 20 ha																							
$Q_{10} = \frac{C \cdot I \cdot A}{360} = \frac{0.50 \times 184 \times 20}{360} = 5.11 \text{ m}^3/\text{s}$																							

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Sec. 2.4.1	Eqn. 2.6	Try with <b>1</b> orifice with diameter <b>1</b> m at same level. Allow head of <b>0.3</b> m from centroid of orifice																			
		<b>B) Determine of Q<sub>riser</sub></b>																			
		$Q_{Riser} = C_o A_o \sqrt{(2gH_o)}$																			
		$= 0.6 \times \frac{1}{4} \times \sqrt{(2 \times 9.81 \times 0.3)}$																			
		$= 1.14 \text{ m}^3/\text{s}$																			
		<b>C) Determine the size of Spillway</b>																			
		$Q_{required} = Q_{10} - Q_{riser}$																			
		$Q_{required} = 5.11 - 1.14$																			
		$Q_{spillway} = C_{sp} B H_p^{1.5}$																			
		Eqn. 2.6		where : Q = emergency spillway discharge (m3/sec) C <sub>sp</sub> = spillway discharge coefficient B = emergency spillway base width (m) H <sub>p</sub> = effective head on the spillway crest (m)																	
Trial spillway dimensions :																					
B = <b>4.00</b> m H <sub>p</sub> = <b>0.90</b> m C <sub>sp</sub> = <b>1.45</b> m																					
$Q_{spillway} = 4.95 \text{ m}^3/\text{sec} > Q_{10} = 3.97 \text{ m}^3/\text{sec} \rightarrow \text{OK!}$																					
<b>D) Trapping Efficiency</b>																					
From previous calculation, The Sediment Yield = 27.80 tonnes for the design storm.																					
Design Sediment Trapping Efficiency of 90% = 25.02 tonnes or 15.64 m <sup>3</sup>																					
The Sediment Storage Capacity is = 4461.6 m <sup>3</sup>																					
No. of Storm Events estimated to fill up the Sediment = 286																					
Assuming the design storm is equivalent to 3-months ARI the Storage zone is likely to be filled up in = 286 Years																					

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**PLAN AND SECTION OF WET SEDIMENT BASIN**

$L_{Top} = 183 \text{ m}$   
 $L_{Base} = 176 \text{ m}$

$W_{Base} = 36 \text{ m}$   
 $W_{Top} = 43 \text{ m}$

$\text{Total water depth} = 1.64 \text{ m}$   
 $\text{Total Basin Depth} = 2.84 \text{ m}$

**SECTION OF EMERGENCY SPILLWAY**

$\text{Width} = 4.0 \text{ m}$   
 $H_p = 0.9 \text{ m}$

*Note:*  
All sketches shown herein are N.T.S