

## APPENDIX C2. DESIGN OF AN ION EXCHANGE COLUMN

### Problem Formulation

Figure C2.1 illustrates the equilibrium data for protein uptake by a cellulose ion exchanger.

Waste water with a protein concentration of 200 mg / l is considered.

The break-point will be considered as the time at which the effluent has a protein concentration of 20 mg / l and the bed will be considered exhausted when the effluent has a protein concentration of 180 mg/l.

$H_t = 0.05$  m

The depth of the ion exchange bed is 0.5 m.

Find  $Z_a$  and the saturation in percentage.

### Solution

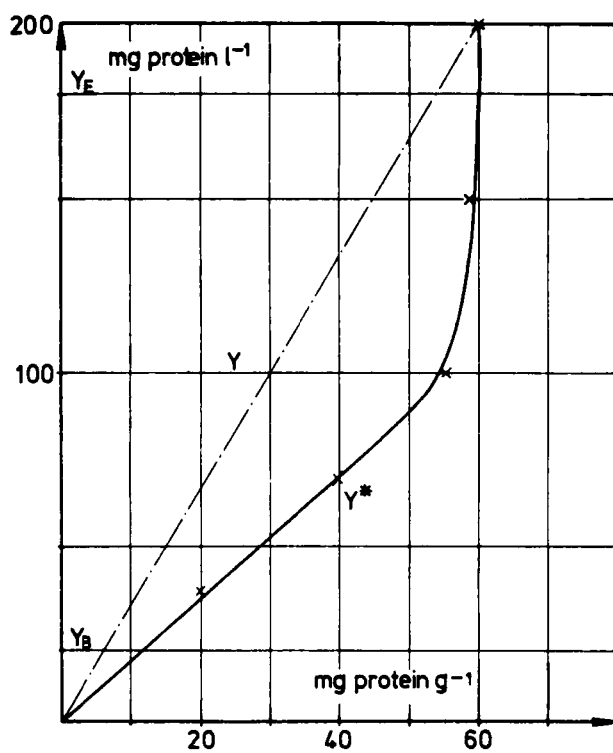
The equilibrium data as indicated above are plotted in Fig. C2.1.. Table C2.1 lists the value of  $Y$  on the operating line between  $Y_b$  and  $Y_E$ , and the corresponding value of  $Y_+$ .

In Table 7.3  $1/(Y-Y_+)$  has been computed. Column 4 in the table is based on Fig. C2.2. and column 5 indicates the corresponding values of  $(W-W_b)/W_A$ .

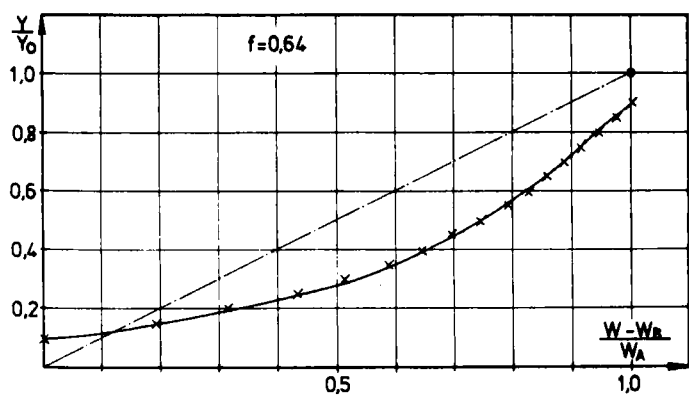
By means of column 6, which shows  $Y/Y_o$ , Fig. C2.3 is plotted. The total number of transferred units is found in Table C2.1 to be 4.23. It is now possible by use of Fig. C2.3. to find  $f$ , as: 0.64.

$$Z_a = N * H_t = 4.23 * 0.05 = 0.21 \text{ m}$$

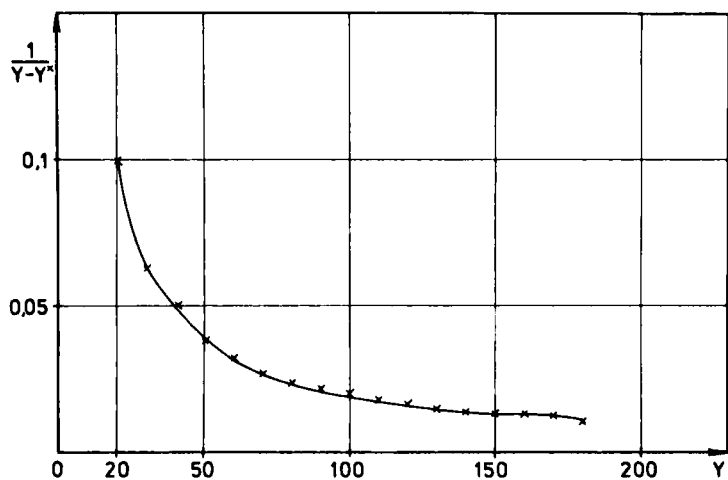
$$\text{Saturation (\%)} = \left( \frac{Z - (1 - f) Z_a}{Z} \right) 100 = \frac{(0.5 - (1 - 0.64) * 0.21) 100}{0.5} = 85\%$$



**Figure C2.1.** Equilibrium line and operation line.



**Figure C2.2.**  $(W - W_B) / W_A = f ( Y / Y_0 )$ .  $f$  can be found to 0.64.



**Figure C2.3.**  $Y = f \left( \frac{1}{Y - Y_x} \right)$

**Table C2.1**

**Theoretical column calculations**

| Y   | Y* | $\frac{1}{Y - Y^*}$ | $\frac{dY}{Y - Y^*}$ | $\frac{W - W_B}{W_A}$ | $\frac{Y}{Y_0}$ |
|-----|----|---------------------|----------------------|-----------------------|-----------------|
|     |    |                     |                      |                       |                 |
| 20  | 10 | 0.100               | 0                    | 0                     | 0.1             |
| 30  | 14 | 0.063               | 0.8                  | 0.189                 | 0.15            |
| 40  | 20 | 0.050               | 1.35                 | 0.319                 | 0.20            |
| 50  | 24 | 0.038               | 1.81                 | 0.428                 | 0.25            |
| 60  | 29 | 0.032               | 2.16                 | 0.510                 | 0.30            |
| 70  | 33 | 0.027               | 2.47                 | 0.584                 | 0.35            |
| 80  | 39 | 0.024               | 2.72                 | 0.643                 | 0.40            |
| 90  | 44 | 0.022               | 2.94                 | 0.695                 | 0.45            |
| 100 | 49 | 0.020               | 3.14                 | 0.742                 | 0.50            |
| 110 | 53 | 0.018               | 3.32                 | 0.785                 | 0.55            |
| 120 | 58 | 0.016               | 3.48                 | 0.823                 | 0.60            |
| 130 | 64 | 0.015               | 3.63                 | 0.858                 | 0.65            |
| 140 | 68 | 0.014               | 3.74                 | 0.884                 | 0.70            |
| 150 | 74 | 0.013               | 3.87                 | 0.915                 | 0.75            |
| 160 | 80 | 0.013               | 4.00                 | 0.946                 | 0.80            |
| 170 | 85 | 0.012               | 4.12                 | 0.974                 | 0.85            |
| 180 | 93 | 0.010               | 4.23                 | 1.000                 | 0.90            |